

Identification of arches in two-dimensional granular packings

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(Received 20 March 2006; published 9 August 2006)

We identify arches in a bed of granular disks generated by a molecular dynamic-type simulation. We use the history of the deposition of the particles to identify the supporting contacts of each particle. Then, arches are defined as sets of mutually stable disks. Different packings generated through tapping are analyzed. The possibility of identifying arches from the static structure of a deposited bed, without any information on the history of the deposition, is discussed.

DOI: [10.1103/PhysRevE.74.021303](https://doi.org/10.1103/PhysRevE.74.021303)

PACS number(s): 81.05.Rm, 81.20.Ev, 83.80.Fg

I. INTRODUCTION

Arches are multiparticle structures encountered in nonsequentially deposited granular beds. In some sense, arches are to granular packings what clusters are to colloids: they represent collective structures whose existence and behavior determine many properties of the system as a whole. During the settlement of a granular bed, some particles come to rest simultaneously by contacting and supporting each other. These mutually stabilized sets of particles are called arches or bridges [1]. Of course, these arches are themselves supported by some of the surrounding particles in the system: the arch bases. Typically, 70% of the particles are part of arches in a granular packing of hard spheres [2]; and around 60% in packings of hard disks [3]. Arch formation is crucial in the jamming of granular flows driven by gravity [4–7] and it has also been proposed as a mechanism for size segregation [8,9].

Arching is the collective process associated with the appearance of voids that lower the packing fraction of the sample. Moreover, arching is directly related to the reduction of particle-particle contacts in the assembly, which determines the coordination number [2,10]. In two dimension (2D), for example, the mean support number $\langle z \rangle_{\text{support}}$ —i.e., the coordination number that accounts only for the contacts that serve as support of at least one grain—can be obtained from the arch size distribution $n(s)$ as [3]

$$\langle z \rangle_{\text{support}} = 2 \left[1 + \frac{1}{N} \sum_{s=1}^N n(s) \right]. \quad (1)$$

Here N is the total number of particles in the packing and $n(s)$ is the number of arches consisting of s grains. The number of particles that do not form part of any arch corresponds to $n(1)$. This mean support number coincides with the mean coordination number $\langle z \rangle$ when the packing does not have any nonsupporting contacts. In nonsequentially deposited beds—especially for soft particles—there will be contacts that are

not essential to the stability of any of the two touching particles.

A systematic study of arching is particularly complex despite the simplicity associated to the concept of arch. The typical structural properties of granular materials are mainly connected with the topological complexity of the contact network. Concepts like “force chain” and “force propagation” have been profusely studied [11], but many open questions still remain. The statistical properties of the arching process could give some insight into these complex problems.

Arches form dynamically during nonsequential particle deposition. Given a settled granular sample, identifying if two particles belong to the same arch is often impossible without knowing the history of the deposition process. Assuming that we are able to identify (experimentally) the contacts of each particle, it is impossible to know which of these contacts are responsible for supporting each particle in place against gravity. For convex hard particles in 2D, only two of the contacts of a given particle provide its stability [in three dimension (3D) this number is three]. The supporting contacts are the first two (three in 3D) contacts made by the given particle that provide stability against the external force that drives deposition (e.g., gravity). Any contact made afterwards will not provide the essential stability assuming that the already formed supporting contacts persist. Of course, if one removes a supporting contact, it is possible that a nonsupporting contact of the particle becomes a supporting contact, hence some nonsupporting contacts may provide secondary (alternative) stability to the particle.

Finding the supporting contacts of a particle is simple in a pseudodynamics simulation approach since these contacts are the essence of the simulation algorithm [2,3,10,12]. However, in a realistic granular simulation—as well as in experiments—one needs to track the particle collisions and analyze stability at every instant to catch the supporting contacts of every particle in the moment they first appear.

In this work, we report a numerical study on the supporting contacts that are created during the nonsequential deposition of a granular bed. Then, arches are straightforwardly obtained and analyzed. We use molecular dynamics simulations and restrict ourselves to a 2D system of inelastic particles in order to reduce the computational cost. We show that our identification of supporting contacts is useful in de-

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ciding when the packing has settled, which is a major issue in these types of simulations. We compare our results with those obtained by pseudodynamics methods. We also show that using simple criteria it is possible to identify arches to some degree without knowing the deposition history. This is of particular interest for experimental studies where tracking particles at high velocities is rather expensive.

II. THE 2D SOFT-PARTICLE MOLECULAR DYNAMICS APPROACH

We simulate the process of filling a box with grains by using a soft-particle 2D molecular dynamics (MD). In this case, the particles (monosized disk) are subjected to the action of gravity. Particle-particle interactions are controlled by the particle-particle overlap $\xi = d - |\mathbf{r}_{ij}|$ and the velocities $\dot{\mathbf{r}}_{ij}$, ω_i , and ω_j . Here, \mathbf{r}_{ij} represents the center-to-center vector between particles i and j , d is the particle diameter, and ω is the particle angular velocity. These forces are introduced in the Newton's translational and rotational equations of motion and then numerically integrated by standard methods [13].

The contact interactions involve a normal force F_n and a tangential force F_t . In order to simplify the calculus we use a normal force which involves a linear (Hookean) interaction between particles.

$$F_n = k_n \xi - \gamma_n v_{i,j}^n, \quad (2)$$

$$F_t = -\min(\mu |F_n|, |F_s|) \text{sgn}(\zeta), \quad (3)$$

where

$$F_s = -k_s \zeta - \gamma_s v_{i,j}^t, \quad (4)$$

$$\zeta(t) = \int_{t_0}^t v_{i,j}^t(t') dt', \quad (5)$$

$$v_{i,j}^t = \dot{\mathbf{r}}_{ij} \cdot \mathbf{s} + \frac{1}{2}d(\omega_i + \omega_j). \quad (6)$$

The first term in Eq. (2) corresponds to a restoring force proportional to the superposition ξ of the interacting disks and the stiffness constant k_n . The second term accounts for the dissipation of energy during the contact and is proportional to the normal component $v_{i,j}^n$ of the relative velocity $\dot{\mathbf{r}}_{ij}$ of the disks. The restitution coefficient is an exponentially decaying function of the dissipation coefficient γ_n [13], i.e., an increase in the dissipation coefficient leads to a nonlinear decline of the restitution coefficient.

Equation (3) provides the magnitude of the force in the tangential direction. It implements the Coulomb's criterion with an effective friction following a rule that selects between static or dynamic friction. Dynamic friction is accounted for by the friction coefficient μ . The static friction force F_s [see Eq. (4)] has an elastic term proportional to the relative shear displacement ζ and a dissipative term proportional to the tangential component $v_{i,j}^t$ of the relative velocity. In Eq. (6), \mathbf{s} is a unit vector normal to \mathbf{r}_{ij} . The elastic and dissipative contributions are characterized by k_s and γ_s , respectively. The shear displacement ζ is calculated through Eq. (5) by integrating $v_{i,j}^t$ from the beginning of the contact

(i.e., $t=t_0$). The tangential interaction behaves like a damped spring which is formed whenever two grains come into contact and is removed when the contact finishes [15].

The model presented above includes all features that turned out to be essential in the work reported here. If only dynamic friction forces are used in the tangential direction, these keep changing slightly *but continuously* once the disks have been deposited, making it impossible to decide whether the deposition process has definitively finished. The addition of static friction forces allows the deposit to reach a stable configuration. Furthermore, apart from the energy dissipation on normal contact, the tangential component is also responsible for energy dissipation through the second term in Eq. (4). This leads to a fast decay of the total kinetic energy of the system whose final value is negligible in comparison with simulations without tangential dissipation.

III. ARCH IDENTIFICATION

To identify arches one needs first to identify the two supporting particles of each disk in the packing. Then, arches can be identified in the usual way [2,3,10]: we first find all *mutually stable particles*—which we define as directly connected—and then we find the arches as chains of connected particles. Two disks i and j are *mutually stable* if i supports j and j supports i .

Regardless of the way grains are deposited, they meet with and split up from other grains until they come to rest. While this process takes place, each time a new contact happens we can check if any of the two touching particles may serve to the stability of the other and save this information. Equally, we can update this data when touching grains come apart. Eventually, when all particles have settled, we should find that every particle has two supporting contacts and that no updates take place any longer. The algorithm that we follow to detect and update supporting contacts is described below.

We consider that two particles in contact with particle i may provide support to it only if the two particles are one at each side of i and the center of mass (c.m.) of particle i is above the segment that joins the two contacts. We call *contact chord* to this segment. For a particle and a wall to support particle i we just need to take into account that the contact between the wall and i has the same y -coordinate as i . A particle in contact with the base is stable per se.

If at any time a particle i has a single contact, we consider this contact as a potential first stabilizing contact (awaiting for the second stabilizing contact to occur) only if i has a higher y -coordinate than the contacting particle. A contacting wall cannot be considered a first stabilizing contact.

We construct two arrays $[nR(i)]$ and $[nL(i)]$ with $i = 0, \dots, N-1$ that store the indices of the *right* and *left* supporting particle of all particles in the system. If a particle has an *undefined support*, the corresponding position in the array is set to -2 . If one of the supporting contacts is a *container's wall* (or base), the corresponding position in the array is set to -1 . Initially, all elements of nR and nL are set to -2 . After an update of all particle positions in the simulation, we check the status of nR and nL , and update them according to the protocol described below. The protocol is repeated until no

case (a) $nR(i) = -1$ $nL(i) = -1$	(1)	$nR(i) = -1$ $nL(i) = -1$	
	(2)	$nR(i) = -2$ $nL(i) = -2$	
case (b) $nR(i) = k$ $nL(i) = j$	(1)	$nR(i) = k$ $nL(i) = j$	
	(2)	$nR(i) = -2$ $nL(i) = -2$	
	(3)	$nR(i) = -2$ $nL(i) = j$	
		$nR(i) = -2$ $nL(i) = -2$	
		$nR(i) = -2$ $nL(i) = -2$	
	(4)	$nR(i) = -2$ $nL(i) = k$	
case (c) $nR(i) = k$ $nL(i) = -2$	(1)	$nR(i) = k$; if i contacts j or wall and the cm is below the contact chord then set $nL(i) = j$ or -1 accordingly	
	(2)	$nR(i) = -2$ $nL(i) = k$	
	(3)	$nR(i) = -2$ $nL(i) = -2$	
	case (d) $nR(i) = -1$ $nL(i) = j$	(1)	$nR(i) = -1$ $nL(i) = j$
		(2)	$nR(i) = -2$ $nL(i) = -2$
case (e) $nR(i) = -2$ $nL(i) = -2$	(1)	$nR(i) = -1$ $nL(i) = -1$	
	(2)	$nR(i) = -2$ $nL(i) = j$	
	(3)	$nR(i) = -2$ $nL(i) = -2$	
	(4)	$nR(i) = j$ $nL(i) = -2$	
	(5)	$nR(i) = -2$ $nL(i) = -2$	

FIG. 1. Schematic representation of the possible states of stability that a particle i can have at any given time (left column) and update protocol that is followed according to the particle position after a simulation step (right columns). The arrays $nR(i)$ and $nL(i)$ store the indices of the disks that support disk i (see text). In case (d-4) we draw a small disk j since this situation is difficult to appreciate by eye for equal-sized disks where small differences in disk-to-wall overlaps are responsible for particle j moving to the right of i .

changes are induced in nR and nL before a new simulation time step is advanced.

There are six different situations that may arise depending on the stability status of a particle previous to the position update. Within each of these cases there are different actions to take depending on the new positions of the particles after the position update. A summary of the most relevant situations is shown in Fig. 1. Not all plausible situations are con-

sidered here because some do not occur in practice or are extremely rare.

Case (a): Here, particle i was resting on the container's base before the position update. We simply check if the particle is still in contact with the base; if not, $nR(i)$ and $nL(i)$ are set to -2 .

Case (b): In this case, particle i was supported (before the position update took place) by two other particles whose

indices are stored in $nR(i)$ and $nL(i)$. We have to check if these particles are still supporting i ; if not, the supporting particles must be redefined according to these possible situations:

(1) $nR(i)$ and $nL(i)$ are still in contact with i , $nR(i)$ is still to the right of i , and $nL(i)$ is still to the left of i , and the c.m. of i is above the contact chord \rightarrow leave $nR(i)$ and $nL(i)$ unchanged.

(2) Neither $nR(i)$ nor $nL(i)$ are in contact with i \rightarrow set $nR(i)$ and $nL(i)$ to -2 .

(3) Either $nR(i)$ or $nL(i)$ is no longer in contact with i \rightarrow set the lost contact to -2 and check that the remaining contacting particle is still on its side (right or left) and below particle i ; if not, set also this contact to -2 .

(4) $nR(i)$ and $nL(i)$ are still in contact with i , but either $nR(i)$ is not to the right of i or $nL(i)$ is not to the left of i \rightarrow say $nR(i)$ is not to the right of i ; then (i) set $nL(i)$ to the contacting particle [$nR(i)$ or $nL(i)$] with lower y -coordinate, (ii) set $nR(i)=-2$.

(5) $nR(i)$ and $nL(i)$ are still in contact with i , $nR(i)$ is still to the right of i , and $nL(i)$ is still to the left of i , but the c.m. of i is not above the contact chord \rightarrow set $nR(i)$ or $nL(i)$ to -2 , the one with highest y -coordinate.

Case (c): This case corresponds to a particle with a first potentially stabilizing contact. Let us assume that this corresponds to $nR(i)$. We have to check that $nR(i)$ is still in place and if any new contact can complete the stability condition. The following situations may arise:

(1) $nR(i)$ is still in contact with i , $nR(i)$ is still to the right of i \rightarrow look for any particle j (or wall) contacting i on its left side such that the c.m. of i is above the contact chord; if any is found, then set $nL(i)=j$.

(2) $nR(i)$ is still in contact with i , but $nR(i)$ is not to the right of i \rightarrow set $nL(i)=nR(i)$ and $nR(i)=-2$.

(3) $nR(i)$ is not in contact with i \rightarrow set $nR(i)=-2$.

Case (d): This case is similar to case (b) but one of the two container's walls takes the place of one of the supporting particles. Let us assume that $nR(i)=-1$, i.e., we are considering the right wall. Again, we have to redefine supporting contacts according to these possible situations:

(1) $nR(i)$ and $nL(i)$ are still in contact with i , $nL(i)$ is still to the left of i , and the c.m. of i is above the contact chord \rightarrow leave $nR(i)$ and $nL(i)$ unchanged.

(2) Neither $nR(i)$ nor $nL(i)$ are in contact with i \rightarrow set $nR(i)$ and $nL(i)$ to -2 .

(3) Either $nR(i)$ or $nL(i)$ is no longer in contact with i \rightarrow (i) set the lost contact to -2 ; (ii) if the remaining contact is $nR(i)$ (the wall), then set $nR(i)=-2$, or else check that $nL(i)$ is still to the left of i and with a y -coordinate below particle i ; if not, set also this contact to -2 .

(4) $nR(i)$ and $nL(i)$ are still in contact with i , but $nL(i)$ is not to the left of i \rightarrow set $nR(i)=nL(i)$ and set $nL(i)=-2$.

(5) $nR(i)$ and $nL(i)$ are still in contact with i , $nL(i)$ is still to the left of i , but the c.m. of i is not above the contact chord \rightarrow set $nR(i)$ and $nL(i)$ to -2 .

Case (e): This case corresponds to a particle i that was in the air (without defined supporting contacts) before the position update. We need to check if any contact has occurred

and if it is a potential first stabilizing contact. Before doing this, we check that the particle has negative vertical velocity to avoid considering particles that are in their way up after a bounce. Two situations may arise:

(1) Particle i contacts the container's base \rightarrow set $nR(i)$ and $nL(i)$ to -1 .

(2) Particle i contacts another particle j \rightarrow if i has higher y -coordinate than j , then set either $nR(i)$ or $nL(i)$ (depending on which side of i is j) to j .

Case (f): This case never arises because a contacting wall cannot be considered a first stabilizing contact.

IV. RESULTS ON TAPPED GRANULAR BEDS

In order to test the algorithm for the identification of supporting contacts and arches in a realistic nonsequential deposition, we carry out MD simulations of the tapping of 512 disks in a rectangular box $13.91d$ wide. The values used for the parameters of the force model are $\mu=0.5$, $k_n=10^5$, $\gamma_n=300$, $k_s=\frac{2}{3}k_n$, and $\gamma_s=200$ with an integration time step $\delta=10^{-4}$. The stiffness constants k are measured in units of mg/d , the damping constants γ in $m\sqrt{g/d}$, and time in $\sqrt{d/g}$. Here, m , d , and g stand, respectively, for the mass of the disks, the diameter of the disks, and the acceleration of gravity. The walls and base are represented by disks with infinite mass and diameter. The velocity-Verlet method was used to integrate the equations of motion along with a neighbor list to speed up the simulation. In order to keep the numerical integration stable, a basic requirement is to use an integration time step δ much smaller than the contact time between particles, which is essentially controlled by γ_n . We have chosen δ to be 50 times shorter than the typical duration of a contact. A more detailed discussion about the numerical algorithm can be found in Ref. [14].

The value of γ_n is chosen deliberately high in order to have a small coefficient of normal restitution ($e_n=0.058$). This way we reduce computer time since fast energy dissipation leads the system to rest in less time. Of course, this also reduces the number of bounces and oscillations in the system.

Disks are initially placed at random without overlaps in the simulation box, and the initial velocities are assigned from a Gaussian distribution of mean zero. The y -coordinates range from 0 up to $100d$. Then, particles are allowed to deposit under the action of gravity. The deposit is said to be stable when the supporting contacts arrays $nR(i)$ and $nL(i)$ (see Sec. III), remain unchanged for 10^4 time steps. Then, the stable configuration is saved. It is worth mentioning that this criterion to decide when the system is "at rest" is very reliable. All our simulation runs end up with unchanging supporting contacts arrays. Even though particles may perform small vibrations about their equilibrium positions and orientations, they remain supported by the same set of particles and this is what defines the mechanical stability in a macroscopic sense.

The tapping process is simulated by moving the container's base and walls in the vertical direction half period of a sine function of amplitude A and frequency $w=2\sqrt{g/d}$. The tapping amplitude is measured through the peak acceleration

$\Gamma = Aw^2$. After all particles have settled down and the stable configuration has been saved, we increase the amplitude of the perturbation by $\Delta\Gamma = 0.0134g$ and the process is repeated. The range of the tapping amplitude goes from 0 to $6.41g$. When the maximum amplitude is reached, the system is then tapped with decreasing amplitudes down to $\Gamma = 0$. Then, a new increasing Γ cycle is started and so on.

The “annealing” protocol is performed several times starting from different initially deposited beds and then the results are averaged separating the very first increasing Γ phase from the rest of the tapping ramps. We introduce this averaging method due to the fact that all quantities obtained for the initial increasing ramp do not match the subsequent decreasing and increasing ramps for amplitudes below some threshold Γ_0 [see the inset of Fig. 3(b)]. The first increasing ramp of the tapping protocol is known as the *irreversible branch* and the subsequent coinciding ramps are known as the *reversible branch*. Despite the introduction of static friction (which could induce history dependent effects) and the fact that we apply a single tap to the system at each Γ , the results show the same trends as many experiments [16–18] where the granular assembly is subjected to some sort of tapped annealing. Unfortunately, the slow decaying time of the compaction process makes it virtually impossible to simulate a real experimental situation.

In order to enhance the quality of the averaged arch properties at given states along the tapping ramp, we take intermediate configurations ($\Gamma = 0.71$ and 4.99) and tap the system at constant Γ for longer runs (1000 cycles). These values of Γ correspond to a high-density and a low-density state of the system. The results obtained from these longer runs are essentially the same as those obtained from the corresponding states along the annealing process; only the statistical dispersion is improved.

We can see two snapshots of configurations obtained at low- and high-tapping amplitudes in Fig. 2. The arches identified in the sample can be appreciated by means of the segments that join mutually stabilizing disks (see Sec. III). A single disconnected segment indicates that the two joined disks support each other and therefore form an arch. A chain of connected segments indicates that all joined disks belong to the same arch. For each arch there are two disks that form the base of the arch, these are not indicated in the figure. The configuration with $\Gamma = 0.71$ [Fig. 2(a)] is quite ordered, showing a localized disordered region at middle height in the packing. Large crystal-like domains of triangular order are observed with clear defect boundaries in agreement with experiments [20]. Here, most arches consist of only two particles; only a few three-particle arches can be appreciated. Figure 2(b) corresponds to $\Gamma = 4.99$. This configuration is clearly more disordered than the former; however, void spaces are rather uniform in size and homogeneously distributed throughout the packing. This contrasts with the larger degree of disorder displayed by pseudodynamic simulations [3] where a wider distribution of void sizes is found. Figure 2(b) shows a larger number of arches than Fig. 2(a), particularly larger arches consisting of up to six disks.

In Fig. 3 we show the results of the mean coordination number $\langle z \rangle$ and packing fraction ϕ obtained for the reversible branch of the tapping ramp (i.e., decreasing ramp). We also

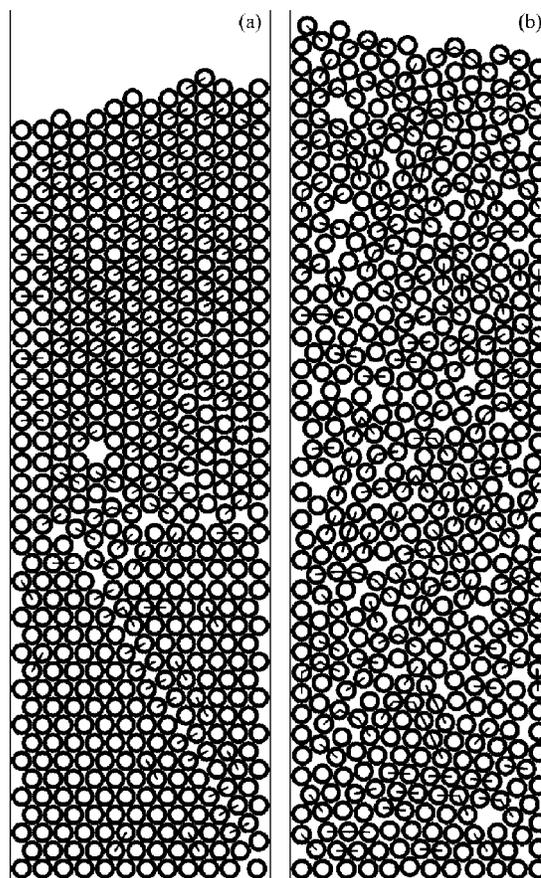


FIG. 2. Two snapshots of the configurations obtained for tapping amplitudes $\Gamma = 0.71$ (a) and 4.99 (b). Arches identified with the protocol of Sec. III are indicated by segments that join disks belonging to the same arch. Note that some disks may seem to be in unstable positions since all contacts are above its center. These disks are in fact stable thanks to the static friction forces. For each arch there are two disks that form the base of the arch (these are not indicated in the figure).

show the values for $\langle z \rangle_{\text{support}}$ that include only those contacts that serve to the stability of at least one of the two touching particles. Unlike hard particles [3], soft particles present more contacts than those just needed to make particles stable, therefore $\langle z \rangle_{\text{support}}$ is not related to $\langle z \rangle$ in a trivial way. We have to bear in mind that $\langle z \rangle_{\text{support}}$ is directly related to the arch size distribution; not $\langle z \rangle$. Our results show that $\langle z \rangle_{\text{support}}$ and $\langle z \rangle$ present qualitatively the same behavior although $\langle z \rangle_{\text{support}}$ presents lower values and varies within a narrower range.

We can see from Fig. 3 that both $\langle z \rangle$ and ϕ have rather high values when the tapping amplitude is small, corresponding to an ordered system. As Γ is increased, those values undergo a slow decrease as the system gets disordered. Finally, ϕ and $\langle z \rangle$ present a slight increase from their minimum values for high tapping amplitudes. This result qualitatively agrees with the experimentally observed behavior in 3D [16] where a minimum in the density dependence on Γ has been observed. However, simulations of disks through pseudodynamics [3] show a much sharper transition between the or-

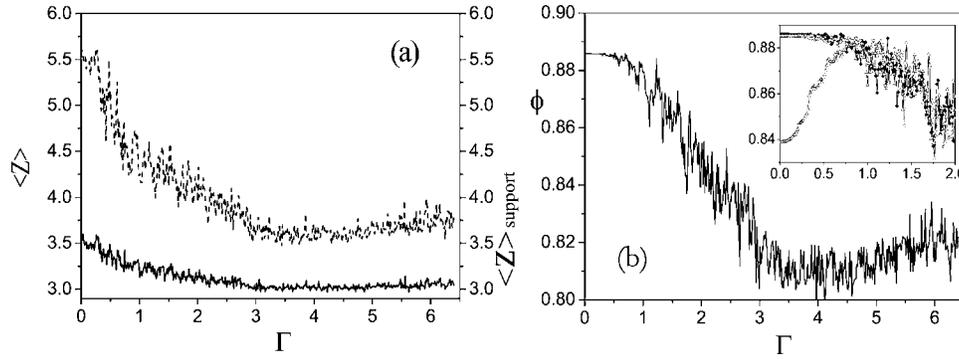


FIG. 3. Coordination number, support number, and packing fraction as a function of the tapping amplitude Γ within the reversible branch of the annealing protocol. (a) Coordination number $\langle z \rangle$ (dashed line) and support number $\langle z \rangle_{\text{support}}$ (solid line). (b) Packing fraction ϕ . The inset in panel (b) shows separately the curves corresponding to several tapping ramps, including the irreversible branch (lower curve).

dered (low Γ) and the disordered (high Γ) regime. Moreover, these simulations [3] present a positive slope in $\langle z \rangle_{\text{support}}$ for low tapping amplitudes within the ordered regime.

Let us look into the relationship between the former quantities and the arches identified by our algorithm. Figure 4 shows the number of arches normalized by the number of particles as a function of Γ along the reversible branch. We see that the large decrease in $\langle z \rangle$ and ϕ (Fig. 3) corresponds to an increase of the total number of arches in the bed. This number reaches a maximum value and then shows a slight decrease in correspondence with the increase in $\langle z \rangle$ and ϕ for high values of Γ . Clearly, there is a correlation between the buildup (breakdown) of arches and the number of contacts and the free volume encountered in the sample. At very low tapping amplitudes the particles deposit in a very ordered manner without forming many arches; this means that, according to Eq. (1), $\langle z \rangle_{\text{support}}$ is rather high (≈ 3.5 , 4 being the maximum allowed value in 2D); moreover, there are few arch-trapped voids and ϕ is high. At moderate Γ , arches are created with high probability; the coordination number then falls accordingly and the arch-trapped voids lower the packing fraction. For very high tapping amplitudes arches are again broken down partially; new particle-particle contacts are created and arch-trapped voids are filled up.

In Fig. 5, the arch size distribution $n(s)$ is shown for two values of the tapping amplitude. We can observe that for moderate tapping amplitudes the system has a larger number of large arches whereas for gentle tapping there is a larger

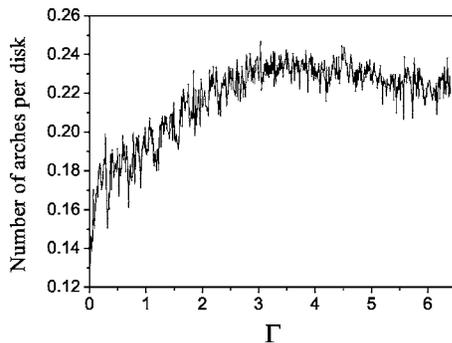


FIG. 4. Number of arches per disk as a function of Γ . Only the reversible branch of the annealing protocol is shown.

amount of disks that do not belong to any arch ($s=1$). Interestingly, in both cases the distribution can be fitted to a second-order polynomial, in a semilogarithmic scale. This is in agreement with results from pseudodynamics simulations [3]. In 3D it has been found that $n(s) \propto s^{-1.0 \pm 0.03}$ [2,10], which corresponds to a significantly higher prevalence of large arches with respect to 2D packings.

In Fig. 6 we show the distributions of the horizontal span of the arches and compare them with a theoretical model [4] based on a restricted random walk. The horizontal span is the projection onto the horizontal axis of the segment that joins the centers of the right-end disk and the left-end disk of an arch. We use the results obtained for arches composed by two, three, and four disks obtained for two different tapping amplitudes. At high packing fractions, arch extensions appear discretized. Since the system presents an ordered layered structure, the particles of any arch of s disks form a string that connects layers (or stay in the same layer) so that the end-to-end horizontal projection of the arch can only be an integer number of on-layer jumps plus an integer number of between-layers jumps; both jumps have characteristic horizontal projections in the triangular lattice formed by the disks. We saw above that although ϕ undergoes a decrease in its value for intermediate tapping amplitudes, it remains rather high. For this reason, although horizontal span distri-

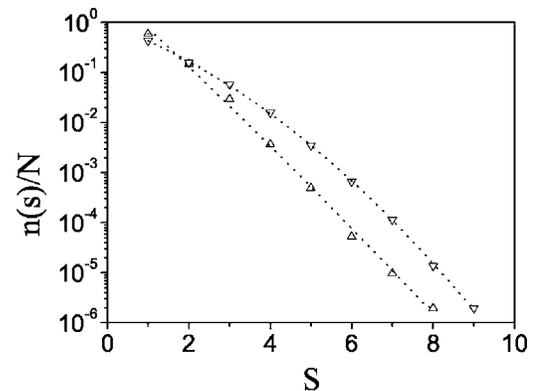


FIG. 5. Distribution of arch sizes for $\Gamma=4.99$ (down triangles) and 0.71 (up triangles). The lines are fits to a second-order polynomial. The data for $s=1$ correspond to the number of disks that are not forming arches.

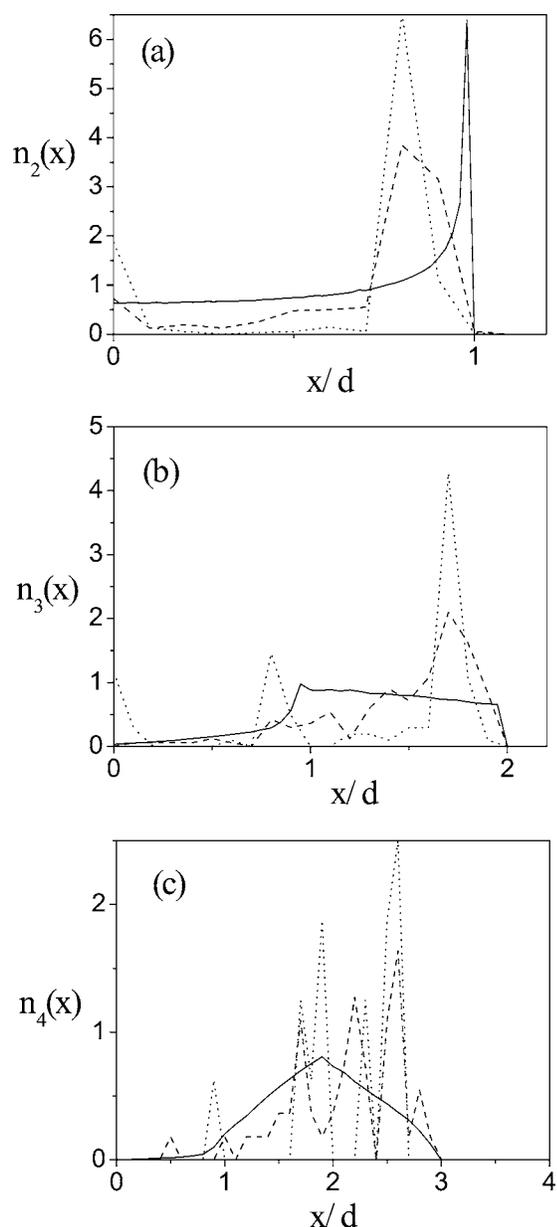


FIG. 6. Horizontal span distribution for arches with 2 (a), 3 (b), and 4 (c) disks. The lines correspond to $\Gamma=0.71$ (dotted) and $\Gamma=4.99$ (dashed). The solid lines correspond to the restricted random walk model [4].

butions are more homogeneous, we still find some characteristic peaks for high Γ . These results do not agree with the prediction of the random-walk model where horizontal span distributions are smooth. However, it must be taken into account that the restricted random walk model was proposed to represent arches at the outlet of a hopper where particles cannot order but simply fit in the gap between walls.

V. ARCHES FROM STATIC CONFIGURATIONS

In this section we intend to show to what extent an attempt to identify arches from the static structure of a deposited system can yield realistic results. We test two criteria

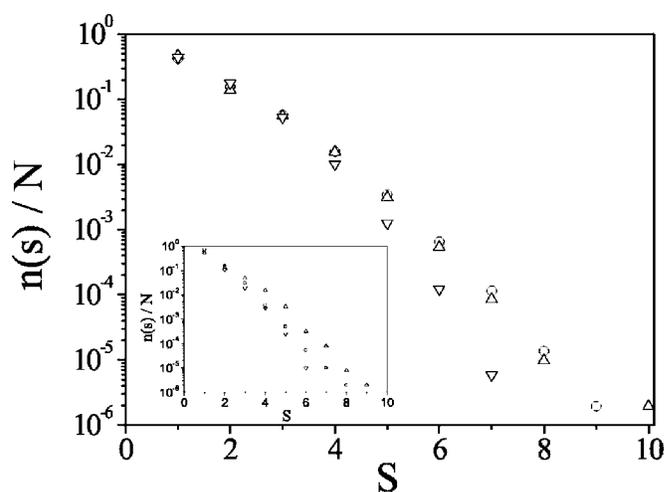


FIG. 7. Distribution of arch sizes for $\Gamma=4.99$ comparing the real distribution obtained from simulations (circles) with the distributions obtained from the static structure using criteria (a) (up triangles) and (b) (down triangles). The inset shows the same results for $\Gamma=0.71$.

that select two of the contacting particles of each particle as the supporting pair of the given grain: (a) *random stabilizing pair*, and (b) *lowest stabilizing pair*. We identify all pairs of contacting particles that may—according to their relative positions and the contact chord criterion—stabilize a given grain. For criterion (a) we then choose one of these pairs at random as the supporting pair. For criterion (b) we choose the pair that has the lower center of mass. In principle, we expect that case (b) should provide a more reliable identification of supporting contacts since those contacting particles in lower positions may correspond to the “real” supports, whereas those in higher positions may correspond to contacts made by further deposition of other particles on top of the particle under consideration. We will see that this is not the case.

We have obtained the arch size distribution $n(s)$ by applying the static criteria above to packings corresponding to $\Gamma=0.71$ and 4.99. Figure 7 shows clearly that, for disordered packings ($\Gamma=4.99$), arches are identified much better by the random criterion. The lowest supporting pair criterion detects less arches than the realistic dynamic criterion. As we can see from the inset of Fig. 7, for very ordered packings ($\Gamma=0.71$), both criteria fail. Criterion (a) overestimates whereas criterion (b) underestimates the number of arches beyond $s=2$. A detailed analysis of the supporting contacts detected by the static criteria shows that criterion (a) tends to find many false mutually stabilizing pair of particles in ordered packings, which leads to the identification of false arches. On the other hand, criterion (b) tends to detect too few of the real mutually stabilizing pairs of particles and for that reason the number of arches detected are fewer than with the dynamic criterion.

VI. CONCLUSIONS AND FINAL REMARKS

We have presented a protocol to dynamically identify arches during the deposition of granular particles carried out

through realistic granular dynamics. We find that simple static criteria can correctly identify arches to some degree for not very ordered packings. In particular, the criterion we call *random stabilizing pair* seems to be the most successful and could be used to identify arches in experimentally generated 2D granular beds [19,20]. However, in ordered packings it is very difficult to identify arches from static configurations. The reason for this is that in an ordered packing the coordination number is rather high and then the number of plausible stabilizing pairs for a given particle is higher than that in disordered packings. Since choosing the correct pair is the essence of the criterion to successfully identify stabilizing contacts, the more pairs we have to choose from, the more likely we make a mistake.

The packings generated by varying the tapping amplitude “quasistatically” present a low-density disordered regime (at high tapping amplitudes) and a high-density, ordered regime (at low tapping amplitudes). The support number decreases with increasing tapping amplitude except for the very high tapping amplitudes. These observations are in contrast with pseudodynamic simulations [3] where $\langle z \rangle_{\text{support}}$ increases with Γ (except at the order-disorder transition). We believe that this is due to the fact that the pseudodynamics is a good representation for fully inelastic disks that roll without slip and that “fall down” at constant velocity—a situation that seems to be met by particles carried on a conveyor belt at low velocities [19]. The simulations in the present work are rather far from this regime since particles can spring away from an impact and so explore a wider range of position in the box before finding a locally stable configuration.

The form of the arch size distributions is in agreement with pseudodynamic simulations. This suggests that the form of $n(s)$ is rather insensitive to the deposition algorithm. The calculated number of arches grows sharply as the density decreases when the tapping amplitude is increased. However, this tendency is not monotonic and above a transition zone the number of arches decreases whereas the density increases. This feature highlights the intuitive connection between arches and density fluctuations.

We have to point out here that the criterion we used to decide if two contacts may be the stabilizing contacts for a given particle i (i.e., that the contact chord is below the c.m. of i), rules out the possibility that a particle be supported from “above.” This situation does indeed arise occasionally due to static friction. Two contacting particles with y coordinates slightly above particle i may sustain the particle due to high static friction forces. We have found that this situation indeed occurs in our simulations. Indeed, some instances can be appreciated in Fig. 2(b). A detailed analysis of these types of arches that are also found in experiments (see, for example, Ref. [4]) will be presented elsewhere.

ACKNOWLEDGMENTS

The authors thank G. C. Barker and A. Garcimartín for useful discussions. This work has been supported by CONICET of Argentina and also partially by the project No. FI2005-03881 MEC (Spain), and PIUNA, University of Navarra. R.A. thanks Friends of the University of Navarra for financial aid.

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